SIGNAL RECOVERY: Sensors, Signals, Noise

and

Information Recovery

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Signal Recovery

COURSE OUTLINE

- • Scenery preview: typical examples and problems of Sensors and Signal Recovery
- \bullet Signals and Noise
- \bullet **Filtering**
- \bullet Sensors and associated electronics

Scenery preview

- \triangleright Elementary view of sensor signal and noise for understanding challenges and problems for the recovery of information
- \triangleright Preliminary overview of typical Resistive Sensors: Thermoresistances and Strain Gauges
- \triangleright Preliminary overview of typical High-Impedance Sensors: Photodetectors for stationary and non-stationary optical signals

Recovery of information from sensors

- • Sensors transduce physical variables (temperature, strain, light etc.) in electrical **signals**
- • Electronic circuits process the electrical signals for recovering the information carried
- •However, sensors and circuits carry also

NOISE

that is, additional random fluctuations of voltage and current

- • If the signal is **NOT much higher** than noise, by collecting the sensor output as it is a degraded information is obtained, affected by significant errors
- • By developing electronic processing tailored to the actual signal and noise such a degradation may be strongly reduced, if not eliminated

Preliminary overview of typical Resistive Sensors: Thermoresistances and Strain Gauges

Sensor case with small signal Thermoresistance or RTD - Resistive Temperature Detector

Principle: resistance variation $(R_0 \Rightarrow R_0 + \varDelta R_0)$ \propto to temperature variation ($T_0 \Rightarrow T_0 + \varDelta T$)

$$
\Delta R = \alpha \Delta T R_o
$$
\n
$$
\Delta T = T - T_o
$$
\n
$$
R_o = R(T_o)
$$

By supplying a **constant** current I_o , a voltage signal is obtained

$$
\Delta V = \alpha \Delta T \cdot V_o
$$

$$
\Delta V = V - V_o
$$

$$
\Delta V = V - V_o
$$

Drawback: the temperature coefficient is very small $\alpha \approx 10^{-3}$ / $^{\circ}$ C hence the signal generated by the sensor is small

Sensor case with small signal Thermoresistance or RTD - Resistive Temperature Detector

The signal is further reduced by the requirement of employing a low voltage supply V_{o} for avoiding to heat the sensor

$$
P = V_o^2 / R_o \qquad \text{typically } R_o \approx 100 \, \Omega
$$

For keeping P < 1μ W it is necessary V_o < 10mV , which gives

$$
\frac{\Delta V}{\Delta T} = \alpha V_o < 10 \mu V / \text{°C}
$$

A variation $\Delta T = 0.01$ °C thus gives a signal $\Delta V < 100nV$. In real cases (e.g. in the control of biochemical reactions) the acceptable errors in the measured temperature are about 0,01 $^{\circ}$ C or even smaller, hence dedicated low-noise amplifier must be employed (ordinary wideband amplifiers have rms noise referred to input typically $\approx 10 \mu V$)

Sensor case with small signal Resistive Sensor of Strain or SG - Strain Gauge

Strain
$$
\varepsilon = \frac{\Delta L}{L_o}
$$
 [measured in unit $\varepsilon = 10^{-6} = 1 \mu \text{strain}$]

Principle : resistance variation \propto to strain

= $G \; \varepsilon R_o \;\;\;$ with fairly small gauge factor G ≈ 2

By supplying a **constant** current I_o , a voltage signal is obtained

$$
\Delta V = G\varepsilon \cdot V_o \qquad \qquad V_o = I_o R_o
$$

$$
\Delta V = V - V_o
$$

Drawback:

the strain to be measured is very small $\varepsilon \approx 1$ to 1000 *ustrain*

(the elastic range of steel is $< 1\%$ i.e $\varepsilon < 10000$ $\mu strain$)

Sensor case with small signal Resistive Sensor of Strain or SG – Strain Gauge

Further drawback:

 V_{o} must be small for avoiding to heat the sensor

$$
P = V_o^2 / R_o \qquad \text{typically } R_o \approx 100 \Omega
$$

For keeping P< 1μ W it is necessary V_o < 10μ V, hence

$$
\frac{\Delta V}{\varepsilon} = GV_o < 20nV/\mu \text{strain}
$$

For instance: with $\varepsilon = 10$ *μstrain* voltage signal $\Delta V < 200$ nV

ordinary amplifiers have much higher rms noise referred to input (typically $\approx 10 \mu V$ for 1 MHz amplifier bandwidth)

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Resistive Sensors with small signal

*invented by Samuel Hunter Christie and popularized by Charles Wheatstone

Wheatstone* Bridge

- • \bullet sensor arm: $\mathsf{R}_{\mathsf{s}1}$ & $\mathsf{R}_{\mathsf{s}2}$
- •• reference arm: $R_{s3}^{}$ & $R_{s4}^{}$
- •differential output signal V_s (differential preamplifier is employed)

Basic configuration:

- •1 sensor R_{s2}
- •• 3 balancing resistors R_{s1} , R_{s3} , R_{s4} R_{s1} = R_{s3} and R_{s4} = R_{s20} (R_{s2o} sensor reference value)
- \Box other configurations of sensors and balancing resistors are also employed
- \Box V_A voltage supply, can be DC or AC

Resistive Sensor with small signal

• A Resistive Sensor is seen by the following circuit as a voltage source of signal with a low resistance in series

- •In various cases the voltage signal is very small
- • A suitably designed **preamplifier** (high input impedance, low-noise, wide- or narrow-band, etc.) has to be coupled to the sensor for picking up the small signal

Resistive Sensor Signal types to be processed

Various types of sensor signals have to be processed, depending

- a) on the behavior of the physical quantity (temperature, etc.)
- b) on the DC or AC bias supply of the sensor
- •For constant physical quantity to be measured we get

with DC bias $\;\rightarrow\;$ DC signal: $\;V_m\;$ with AC bias $\;\rightarrow$ AC signal: $\;V_m^{}$ cos ωt

• For slowly varying physical quantity we get

with DC bias $\;\rightarrow\;$ slowly varying signal: $\;V_m(t)$ with AC bias $\;\rightarrow\;$ modulated AC signal: $\mathit{V}_{m}(t) \mathrm{cos}(\omega t)$

The signal must picked up by a specifically designed preamplifier (low-noise, high input impedance, wide- or narrow-band, etc.)

Preliminary overview of typical High-Impedance Sensors: Photodetectors

Principle:

- Light directed onto a reverse-biased p-i-n junction
- \triangleright 1 absorbed photon \rightarrow 1 free charge carrier (hole-electron pair)
- \triangleright Free carriers driven by electric field travel in the junction
- \triangleright Signal current flows at PD terminals

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- • A photodiode is seen by the following circuit as a current-source with a very high-resistance in parallel
- \bullet The current signal from the source is VERY SMALL

Let's consider first a versatile **wide‐band** circuit configuration

- •**• Low resistance** load, e.g. R_L = 1kΩ
- •• Low capacitance load, e.g. C_{L} = 1pF
- Preamplifier with wide-band (e.g. 100MHz) and low-noise

 \triangleright In this case the resistor R_L is the dominant noise source and causes \cong 40 nA current noise referred to the preamp input

- \triangleright The signal current I_s has to be compared with such noise
- \triangleright The optical signal is small; moreover not all incident photons are absorbed and contribute to *Is* (Photon Detection Efficiency PDE < 1)
- \triangleright A suitably designed preamplifier has to be coupled to the sensor for picking up the small signal
- **Various types of optical signals** are met in the applications: stationary or modulated, single pulse, repetitive pulses

Sensor case with small signal: Photodiode (PD) with **Stationary** light signal

cases with stationary optical power $P^{}_{L}$ = constant Continuous Wave (CW) light sources: LEDs, Lasers, etc.

- \bullet • Measurements are required down to very low $P_L < 100$ nW *(for comparison: ^a red laser pointer has PL [≈]1mW)*
- P_{L} = 100nW of red light (λ = 612nm) corresponds to: $n_p \approx 3 \cdot 10^{11}$ photons/s = 300 photons/ns
- The signal current *I_s* thus generated is small, comparable to noise also in case of PDE= 100% : *Is* [≈] 50nA

light signal with **modulated** optical power

 P_L = $P_{L m}$ cos $\omega_m t$ + $P_{L \vec{o}}$ *modulated* power $P_r = P_r$ $\cos(\theta) + P_r$ \longleftarrow *mean power*

- • The information is entrusted to a modulated light signal for distinguishing the signal from background light and other unwanted sources and for better extracting the signal from noise (note that $P_{Lm} < P_{Lo}$: the modulated power P_{Lm} is lower than the mean power P_{Lo} , *the total optical power PL can't be negative)*
- • The signal generated by the sensor thus includes a modulated current I_S = I_{Sm} cos $\omega_m t$ + I_{So}
- •• very small modulated current *I_{sm}* can be measured, even much lower than the total current noise referred to the preamp input
- •• measurement of P_{Lm} can thus be carried out down to power level quite lower than in cases with steady power $P_{_L}$ (CW cases)

Sensor case with small signal: Photodiode (PD) **Single‐pulse** light signal

The INFORMATION is carried by the AMPLITUDE A_{p} of a light pulse.

Such a case is met in various applications, e.g. in biomedical and genetic analysis.

Example: Flow Cytometry

- •single cells travel in fluid flow system and cross a laser beam;
- \bullet the laser excites fluorescence in the cell;
- • the fluorescence intensity carries information about the cell. The scattered laser light background is blocked by optical filters, the fluorescence is detected by a PD

NB1: just the MAGNITUDE of the pulse matters, NOT THE WAVEFORM

- \bullet Therefore, high-fidelity amplification is NOT required
- •filtering that modifies the pulse shape can be employed

NB2: if pulses occur in sequence EACH pulse must be INDIVIDUALLY measured

Sensor case with small signal: Photodiode (PD) **Repetitive‐pulse** light signal

The pulse carrying INFORMATION is repeated in sequence and ALL the pulses in the sequence carry THE SAME information.

Example: reflectometry

- •Laser pulses are directed to a target
- •Reflected pulses are detected and their size carries info about the target

The redundant information available can be exploited by means of measurements that SUM (or average) the amplitude of ALL THE PULSES

Photodiode: it is almost a current-source (very high-resistance source) of small current signals

A suitable high load $R^{\vphantom{\dagger}}_{\scriptscriptstyle{L}}$ and a specifically designed low-noise preamplifier must be employed, depending on the measurement required

Set-Up for Sensor Measurement

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